

# APPLICATION UNDER UNITED STATES PATENT LAWS

Invention: **METHOD AND APPARATUS FOR PROCESSING  
INTERAURAL TIME DELAY IN 3D DIGITAL AUDIO**

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## This is a:

- ☐ [ ] Provisional Application
- ☒ [X] Regular Utility Application
- ☐ [ ] Continuing Application
- ☐ [ ] PCT National Phase Application
- ☐ [ ] Design Application
- ☐ [ ] Reissue Application
- ☐ [ ] Plant Application

## **SPECIFICATION**

09190208-111398  
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# METHOD AND APPARATUS FOR PROCESSING INTERAURAL TIME DELAY IN 3D DIGITAL AUDIO

This application claims priority from U.S. Patent Application  
5 No. 60/065,855 entitled "Multipurpose Digital Signal Processing System"  
filed November 14, 1997, the specification of which is explicitly  
incorporated herein by reference.

## BACKGROUND OF THE INVENTION

### 10 1. Field of the Invention

This invention relates generally to three dimensional (3D)  
sound. More particularly, it relates to a digital implementation of interaural  
time delays used in 3D digital sound applications.

### 15 2. Background of Related Art

Many high-end consumer devices provide the option for  
three-dimensional (3D) sound, allowing a more realistic experience when  
listening to sound. In some applications, 3D sound allows a listener to  
perceive motion of an object from the sound played back on a 3D audio  
20 system.

Atal and Schroeder established cross-talk canceler  
technology as early as 1962, as described in U.S. Patent No. 3,236,949,  
which is explicitly incorporated herein by reference. The Atal-Schroeder  
3D sound cross-talk canceler was an analog implementation using  
25 specialized analog amplifiers and analog filters. To gain better sound  
positioning performance using two loudspeakers, Atal and Schroeder  
included empirically determined frequency dependent filters. Without  
doubt, these sophisticated analog devices are not applicable for use with  
today's digital audio technology.

Interaural time difference (ITD), i.e., the difference in time that it takes for a sound wave to reach both ears, is an important and dominant parameter used in 3D sound design. The interaural time difference is responsible for introducing binaural disparities in 3D audio or acoustical displays. In particular, when a sound object moves in a horizontal plane, a continuous interaural time delay occurs between the instant that the sound object impinges upon one of the ears and the instant that the same sound object impinges upon the other ear. This ITD is used to create aural images of sound moving in any desired direction with respect to the listener.

The ears of a listener can be 'tricked' into believing sound is emanating from a phantom location with respect to the listener by appropriately delaying the sound wave with respect to at least one ear. This typically requires appropriate cancellation of the original sound wave with respect to the other ear, and appropriate cancellation of the synthesized sound wave to the first ear.

Atal-Schroeder implemented the delays and cancellations with appropriate analog filters and analog amplifiers, as shown herein in Figs. 5 and 6. Figs. 5 and 6 herein are described in detail in the Atal-Schroeder U.S. Pat. No. 3,236,949 with reference therein to Figs. 2 and 4, respectively. Fig. 5 herein shows the conventional 3D sound system for creating the image of sound from a phantom locality with respect to the listener, while Fig. 6 herein shows the analog delay line with multiple tap points implemented by Atal-Schroeder.

Thus, the interaural time delay is manipulated to synthesize localities of the source of particular sounds, and to create the sense of motion of particular sounds.

Conventional 3D sound systems embed the interaural time difference in empirically determined head-related transfer functions (HRTFs), typically determined with a mannequin head implanted with

microphones in its ears. The available delays typically have a relatively large resolution, e.g., 100 microseconds, formed by null filter taps, as disclosed by Atal-Schroeder.

However, there are at least two basic problems with the implementation of the conventional analog approach in a digital environment. First of all, the large resolution in the available time delays cause discretely sampled interaural time differences for the expected position of a listener. Thus, a 'closest' or 'best fit' ITD must be chosen, which may be up to 50% away from the ideal parameter. This may cause a jittering effect in the sense of movement of the sound by the listener. Moreover, implementation of a digital filter emulating the analog filter having multiple taps as shown herein in Fig. 6 is computationally involved, providing a level of system inefficiency from a computational view.

One conventionally proposed implementation of a digital 3D sound system to provide a more accurate ITD based on the given resolution has been to interpolate the entire HRTF set such that the ITD becomes interpolated as well. Unfortunately, interpolation itself can become a computationally intense requirement which likely adds to, rather than cures, the computational inefficiency otherwise associated with digital 3D sound systems.

There is thus a need for an efficient and simplified method and apparatus for providing digital 3D sound.

### SUMMARY OF THE INVENTION

In accordance with the principles of the present invention, a digital delay line for use in a 3D audio sound system comprises a first delay module providing a choice of any delay within a first resolution. A second delay module is in series with the first delay module. The second delay module provides a choice of any of a plurality of additional fractional

delays. Each of the additional fractional delays is less than the first resolution.

A method for providing an interaural time delay in a digital 3D sound system in accordance with another aspect of the present invention comprises selecting one of a plurality of available first time delays having a first resolution between each of the plurality of available first time delays. Additionally, one of a plurality of available second time delays is selected. Each of the plurality of available second time delays is less than the first resolution. The selected first time delay is added to the second time delay to provide a desired interaural time delay.

### **BRIEF DESCRIPTION OF THE DRAWINGS**

Features and advantages of the present invention will become apparent to those skilled in the art from the following description with reference to the drawings, in which:

Fig. 1 is a block diagram showing the digital 3D sound system including a digital interaural delay line, in accordance with the principles of the present invention.

Fig. 2 is a more detailed diagram showing the digital 3D sound system for creating 3D sound in a digital environment, in accordance with the principles of the present invention.

Fig. 3 is a diagram showing the implementation of multiple digital audio streams using a common bank of fractional delay filters, in accordance with the principles of the present invention.

Fig. 4 shows a process for creating an improved ITD look-up table suitable for use in an ITD look up table for use with 3D sound applications as shown in Figs. 1 and 2, in accordance with the principles of the present invention.

Fig. 5 shows a conventional 3D sound system for creating the image of sound from a phantom locality with respect to the listener.

Fig. 6 shows a conventional analog delay line with multiple tap points implemented by Atal-Schroeder.

## DETAILED DESCRIPTION OF ILLUSTRATIVE EMBODIMENTS

5 In accordance with the principles of the present invention, the ITD is extracted from measured and empirically determined HRTFs, smoothed, and implemented in a look-up table. Implementation of the ITD is provided by a delay line including both an integer portion providing rough estimate delays and a fractional portion providing a very accurate  
10 delay and eliminating discontinuities in the listening field to provide a more relaxed listening sweet spot.

The present invention provides a digital filter bank having a simple and inherently low cost architecture for performing a stable cross-talk cancellation, providing excellent localization and externalization of  
15 virtual sound images.

In accordance with the principles of the present invention, head-related transfer functions corresponding to the speaker positions are recorded and used to construct the filter coefficient. The relationship between the speaker position and filter design were studied to provide a  
20 more relaxed listening "sweet spot" where the 3D sound effects are optimized. Thus, the listener does not have to sit in a very accurately placed position with respect to the loudspeakers to appreciate the 3D aspects of the audio rendered by only two loudspeakers.

Fig. 1 is a block diagram showing the basic components of  
25 the disclosed embodiment of a digital 3D sound system including a digital interaural time delay line, in accordance with the principles of the present invention.

In particular, a sound source **220** is input into a digital interaural time delay line **254**. the interaural delay line **254** includes an  
30 integer delay module **250** providing a rough estimate of the desired

interaural time delay, and a fractional delay module **252** providing a highly refined additional time delay. In the disclosed embodiment, both the particular settings of both the integer delay module **250** and the fractional delay module **252** are chosen from among a plurality of predetermined delays, greatly reducing or eliminating the otherwise intensive calculations necessary to interpolate a particular interaural time delay.

The particular delay associated with the left (or right) ear signal **260** and the right (or left) ear signal **262** providing the desired localization of the sound image is provided by a localization control module **270**.

Fig. 2 is a more detailed diagram showing the digital 3D sound system shown in Fig. 1.

In particular, the integer delay module **250** of the disclosed embodiment is comprised of a first-in, first-out (FIFO) buffer **204**. The FIFO buffer **204** may be of any suitable width, e.g., 16 bits, corresponding to the length of the digital audio samples. Moreover, the length of the FIFO buffer **204** will be based on the largest delay necessary to implement the desired 3D sound imaging. The particular delay is related to the selected number of clock cycles after the particular digital audio sample was input to the FIFO buffer **204**. This selection of an integer delay time is represented in Fig. 2 with a multiplex switch **206**. The use of any of the particular digital audio samples **224a-224d** are fed serially into the FIFO buffer **204**, with the arrows from each of the samples **224a-224d** representing tap numbers.

The clock cycle of the FIFO buffer **204** relates to one over the sample rate. Thus, with an exemplary sample rate of 22 kiloHertz, the 'integer' portion, or resolution of the integer delay module **250** is 1/22,000 or approximately 45 microseconds (uS).

The second portion of the digital interaural delay line **254** provides a much more refined 'fractional' delay with a fractional delay

module **252**. This fractional delay is provided by the selection of any one of a plurality of fractional delay filters **208-212**.

5 The fractional delay module **252** effectively produces an adjustable digital delay with a finer resolution than the integer delay module **250**. Each of the fractional delay filters **208-212** is a so-called all-pass filter that has a variable phase shift, corresponding to the required fractional delay. The number of phases (i.e., fractional delay filters **208-212**) is determined empirically by behavioral testing of human listening.

10 In the disclosed embodiment, 64 fractional delay filters are utilized, each providing an incrementally greater delay, in finely resolved increments suitable to the application. For instance, at the exemplary sample rate of 22 kiloHertz, the resolution between the fractional delay filters **208-212** is (45 uS)/64, or about 0.7 uS resolution. This particular fine resolution (and the rough estimate resolution provided by the integer delay module **250**) can be adjusted based on the needs of the particular application.

15 Each fractional delay filter **208-212** is a finite impulse response (FIR) filter, i.e., a polyphase filter, effecting the desired delay. Each of the fractional delay filters **208-212**, and/or the fractional delay controlled switch **216** and/or the multiplexer **214** can be implemented in any suitable processor, e.g., in a digital signal processor (DSP), microprocessor, or microcontroller. Alternatively, the digital filters can be implemented in hardware in accordance with the principles of the present invention.

25 In the exemplary embodiment utilizing a sampling rate of 22 kiloHertz, the first fractional delay filter **208** provides 0.7 uS delay to a digital audio sample passing therethrough, the second fractional delay filter **210** provides approximately 1.4 uS delay, etc., until the last fractional delay filter **212** which provides approximately 44.3 uS delay.



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Selection of the appropriate fractional delay filter **208-212** is implemented by a multiplexer **214** in the fractional delay module **252**. In the shown embodiment, the fractional delay filters **208-212** are each implemented in a processor, e.g., in a digital signal processor, and  
5 selection of an appropriate one of the fractional delay filters **208-212** is desirable at the front end to avoid wasted computational power by running fractional delay filters **208-212** which are not being used for that particular audio sample.

The interaural time delay is controlled by the localization  
10 control module **270**, which includes a 3D audio application source position controller **222**, an interaural time delay (ITD) look-up table **220**, and an integral and fractional delay selector **218**. In the disclosed embodiment, the localization control module **270** is implemented in a suitable processor, e.g., in a microprocessor, microcontroller, or digital signal  
15 processor (DSP). Of course, the localization control module **270** may alternatively be partially or wholly implemented in hardware, e.g., using programmable array logic.

The 3D audio application source position control **222** selects a desired 'phantom' position of the sound sample currently being input to  
20 the digital interaural delay line **254**. The desired location may have a desired x, y and z coordinate with respect to a reference point, e.g., the center of the listener's head. Based on the desired location, an associated ITD is determined in the ITD look-up table **220**. The integral and fractional delay selector determines the largest integer value which  
25 can be achieved within the resolution of the integer delay module **250** without exceeding the desired ITD, and appropriately controls the integer delay module **250** to provide that desired delay to the audio sample. Similarly, the remainder or fractional portion of the desired ITD which is not provided by the integer delay module **250** is provided by an

appropriate selection of a desired one of the available fractional delay filters **208-212** in the fractional delay module **252**.

Fig. 3 is a diagram showing the implementation of multiple digital audio streams using a common bank of fractional delay filters, in accordance with the principles of the present invention. Thus, the plurality of fractional delay filters **208-212** can be utilized by a plurality of audio sources for the same listener, avoiding the need to duplicate the fractional delay module **252** for each audio source.

Fig. 4 shows a process for creating the ITD look-up table **220** shown in Fig. 2.

In particular, in step **102**, binaural impulse responses are empirically measured with a sound source at various locations around the listening environment, e.g., at incremental points along a sphere about the sound source.

In step **104**, the ITD information is extracted from the empirically measured information obtained in step **102**, and a 'mesh' of ITD values for each appropriate point on the sphere is determined. In particular, the ITD samples may be extracted from measured left-right ear head-related transfer functions (HRTFs) using cross-correlation. These samples can be viewed as discrete samples of an underline continuous ITD function of azimuth and elevation coordinates.

In step **106**, to avoid the 'jittering' and other undesirable effects for the listener, the ITD mesh determined in step **104** is smoothed using any appropriate smoothing algorithm. For instance, the ITD samples may be regularized using a "generalized spline model" or appropriately filtered and interpolated by a two-dimensional filter to gain smoothness and continuity. While this smoothing may be calculation intensive, it is performed once, off-line, and not performed in real-time as digital audio samples are received.

In step **108**, the smoothed ITD mesh is input into the ITD look-up table **220**. The ITD mesh may utilize any appropriate coordinate system, e.g., spherical coordinates or a standard x, y and z coordinate system.

5 In the disclosed embodiment it was determined that the finest time resolution of the overall delay, i.e., the combination of the delay provided by the integer delay module **250** and the fractional delay module **252**, is preferably less than 1 microsecond ( $\mu$ S) such that any discontinuity caused in the sound stream is under the hearing threshold of  
10 a typical human. In the case of a high sampling rate, faster time resolution may be preferred. For example, with a 22.05 kiloHertz sampling rate of an audio stream, a 64-phase polyphase filter was used to obtain sub-microsecond resolution in the time delay. In another example, a 60-phase polyphase filter was used to provide the necessary time  
15 delays for a suitable presentation of a audio stream sampled at 48 kiloHertz.

While the fractional delay filters **208-212** in the disclosed embodiment are each a FIR (polyphase) filter, the principles of the present invention are equally applicable to the use of other filters or digital  
20 delays which provide the required delay in a digital audio sample.

The digital interaural delay line **254** in accordance with the principles of the present invention can be implemented in any suitable processor or computer system. For instance, the digital interaural delay line **254** can be implemented at a host level in a personal computer (PC)  
25 based platform using regular instruction sets or MMX™ technology, or can be implemented in a digital signal processor (DSP).

To further improve upon efficiency in accordance with the principles of the present invention, the delay may be fixed for one ear, and varied for the sound intended for the other ear, according to the desired  
30 movement of the source sound. This alternative method may save as

many as half of the instruction cycles required to otherwise process a variably delayed sound to both ears.

The appropriately delayed left and right ear signals can be forwarded to a next stage for further processing, or sent directly to  
5 headphones or loudspeakers for presentation to the listener, as a simple binaural signal processing method.

Thus, in accordance with the principles of the present invention, a solution to the problem of generating a proper interaural time delay in 3D audio and acoustical virtual display applications is  
10 implemented with the requirement for little processing delay. The principles of the present invention saves instruction cycles of a processor over conventional interpolation techniques, and use of the FIFO buffer **204** eliminates the need for the storage of a suitable plurality of null taps in each of the many otherwise required conventional HRTF filters. The  
15 saved processing power can be used for other purposes, e.g., to enhance the HRTF effects.

Since ITDs are extracted, processed, and implemented separately in a roughly resolved delay module (i.e., the integer delay module **250**), and in a finely tuned delay module (i.e., the fractional delay  
20 module **252**), the 3D audio effects can be easily controlled and adjusted to suit other special requirements, e.g., to be optimized for different head sizes. The super resolution sub-sample filtering polyphase filter based delay lines in accordance with the principles of the present invention introduce necessary delay without introducing discontinuity or 'clicks' in  
25 the presentation to the listener.

The principles of the present invention are applicable for use in any 3D audio system that uses an interaural time delay as a localization queue for perceived direction of the sound by the listener. For instance, the present invention relates to 3D sound positioning in gaming,  
30 virtualizing multiple loudspeaker array systems having two physical

speakers in AC3/Dolby™ Digital systems, advanced computer user interfaces, virtual acoustic reality software for architectural walk-throughs, auralization hardware/software, 3D enhancement for general stereo and wireless headphone sets, etc.

- 5           While the invention has been described with reference to the exemplary embodiments thereof, those skilled in the art will be able to make various modifications to the described embodiments of the invention without departing from the true spirit and scope of the invention.